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Interfacial tension for various organic-water systems and study of the effect of solute concentration and temperature

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Abstract

Interfacial tension is an important thermophysical property for the operations involving multi fluid-phases such as liquid-liquid extraction. This work aims at presenting a rapid experimental method and initial interfacial tension data of 10 organic compounds and water binary systems. The organic compounds include n-butyl acetate, cyclohexanol, cyclohexanone, diethyl ether, ethyl acetate, methyl ethyl ketone, methylcyclohexane, 1-octanol, and toluene. The effect of temperature on the initial interfacial tension has also been studied. These systems are chosen to cover a wide range of interfacial tension (1–51 mN/m). Comparisons between the data sets from this work and those from the literature, whenever available, show generally very good agreement. This work also presents new data of initial interfacial tension for several ternary systems with 4 organic compounds and water with varying quantities of propionic acid (0 to 0.25 mass fraction) at ambient conditions; the organic compounds include n-butyl acetate, cyclohexanone, 1-octanol, and toluene. The results show that the impact of propionic acid concentration as solute in water is large, especially at the higher solute concentrations. The initial and final (mutually saturated phases) interfacial tensions are found in agreement for different immiscible binary systems studied in this work. The method presented may be used as a rapid way of finding interfacial tensions.

Keywords

Initial interfacial tension, drop weight method, liquid-liquid extraction, propionic acid, water-organic system.

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Introduction

Interfacial tension is defined as the change in Gibbs free energy per unit change in interfacial area for the two immiscible phases such as liquid-liquid or gas-liquid¹. Interfacial tension in liquid-liquid systems plays an essential role in the analysis and design of the equipment used in liquid-liquid contacting systems such as liquid-liquid extraction. It greatly affects the hydrodynamics and mass transfer behavior of a liquid-liquid extractor. For example, a low interfacial tension system is characterized by small size dispersed phase droplets that may increase the dispersed phase holdup as well as the mass transfer efficiency². On the other hand, low interfacial tension may lead to foaming in certain cases that may or may not be desired. Interfacial tension of a liquid-liquid system may vary significantly in the presence of a solute that influences the working and design of the liquid-liquid extractor. Along the length of a typical column type extractor, solute concentration varies in both the phases; this variation results in a variable interfacial tension along the height of the column. A better understanding of the relationship between solute concentration and interfacial tension may therefore be essential for the operation and design of a liquid-liquid extractor^{2,3}. Interfacial tension may vary with temperature that may also affect the performance of the extractor.

Interfacial tension for binary systems such as water-organic systems has been studied by a number of researchers⁴⁻²⁶. Demond and Lindner¹ and Freitas et al.²⁷ have presented excellent reviews in the literature. The interfacial data are generally determined at near-ambient conditions; the effect of temperature on the interfacial tension of a system has rarely been reported in the literature. Also, the data of multicomponent systems, i.e., in the presence of a solute are scarce¹³.

For sparingly-soluble biphasic systems, the initial interfacial tension (without reaching equilibrium) and equilibrium interfacial tension are same; often different researchers do not explicitly mention if both the liquids are saturated with each other before the measurements or not. In a typical measurement, interfacial tension (and densities) of the mutually saturated phases (equilibrated phases) should be reported. Calculation of interfacial tension often requires densities of saturated phases. Initial interfacial tension can be different from final or equilibrium interfacial tension or simply interfacial tension as it does not require saturation of the phases; it also uses the densities of pure components for the calculation purposes. No water would be dissolved in the organic phase and vice versa. During the measurement, the water droplet is exposed to the organic phase which could lead to a gradual ongoing saturation in both the phases. The same holds for the ternary systems studied. Because all the experiments are concluded in a relatively shorter time span in our work, therefore it is expected that amounts of solutes transferred between two phases are negligibly small.

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3 Here, the interfacial tension is based on virtually pure component interactions and not on the
4 interactions between the mutually saturated phases. This type of interfacial tension (initial
5 interfacial tension) may be important in the startups and in the sections near the inlet and outlet
6 of an extraction column.
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10 In the present study, initial interfacial tensions of ten binary aqueous-organic systems are
11 experimentally determined and the variations in initial interfacial tensions of the selected
12 aqueous-organic systems with the variation in temperature and propionic acid (solute)
13 concentration in the aqueous solution are studied. Apparently, no other initial interfacial tension
14 data seem to be available for the systems studied in the present work. Industrially propionic acid
15 is produced via hydrocarboxylation of ethylene in the presence of water using nickel carbonyl as
16 the catalyst. Numerous industrial applications of propionic acid involve water that warrants study
17 of its aqueous ternary systems with selected organic compounds.
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21 While we selected propionic acid as a representative carboxylic acid due to the fact that it is
22 often found in aqueous forms in a number of industrial and natural processes, the main purpose
23 of selecting it is the fact that the systems studied in this work are not reported earlier.
24 Furthermore, we have covered a large range of interfacial tension by selecting a variety of binary
25 and ternary systems including those with propionic acid. We are aware of the fact that the
26 propionic acid will likely change intermolecular interaction perhaps due to pH change of the
27 water phase that can be one of the reasons of the changes in interfacial tension with
28 concentration, nevertheless, this work reports useful quantitative data of these changes. We
29 studied a fairly large range of propionic acid concentrations -starting from very low to fairly
30 high- to be consistent with our earlier objective, i.e., covering a wide range of interfacial tension.
31 Because propionic acid is often encountered in its aqueous solutions therefore we find it relevant
32 and useful.
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42 **Experimental**

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44 The drop weight method^{1,4,5,8} is used to determine the initial interfacial tension. In the drop
45 weight method, the weight of the heavier phase drop becomes equal to the interfacial force that
46 occurs at the interface of the phases involved and the weight of the drop is a measure of the
47 interfacial tension. The drop of one liquid phase formed by tubing detaches and falls into the
48 body of the other liquid phase. Measuring the weight of the drop and the tubing radius provide
49 the magnitude of the interfacial tension present between the two liquid phases. As the
50 detachment is not perfect therefore a correction factor is required to balance the gravity and the
51 interfacial tension forces.
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3 By initial interfacial tension, as discussed earlier, we mean that the phases are not mutually
4 saturated or equilibrated before the actual measurement. All efforts are made to make sure that
5 the measurements are conducted at a slow pace to avoid experimenter's influence; the
6 measurements are concluded during the initial phase of equilibration between two phases.
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10 Fig. 1 shows a purpose-built equipment constructed, calibrated, and used in this work. It
11 mainly consisted of a cylindrical glass cell and a pre-calibrated and graduated 1.0 cm³ syringe
12 fitted with a removable stainless steel needle (Rudolph Research Analytical, product number
13 P23897) with clean-cut tip perpendicular to the bore of known inside and outside diameters,
14 verified using a screw gauge with least count ± 0.01 mm. The inside diameter of the needle was
15 1.06 mm while the outside diameter was 1.60 mm. The internal diameter was verified by a set of
16 stainless-steel wires with known, gradually-increasing and uniform diameter. The uncertainty
17 associated with the representative needle diameter and that associated with the droplet volume
18 show acceptable influence (within the standard deviation of quadruplicates) on the interfacial
19 tension data reported in this work. In order to maintain the temperature of measurement, the
20 cylindrical cell was placed inside the water thermostat. The temperature was maintained with
21 ± 0.25 K, measured by a mercury thermometer with least count within temperature stability of
22 0.25 K. A purpose-built screw assembly was provided to drive the syringe plunger by which it
23 was possible to move the syringe plunger at a sufficiently slow pace so that the correct size of the
24 drop was produced.
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34 In a typical procedure, the cell was partially filled with the lighter phase (organic phase) and
35 the heavier phase (aqueous phase) was allowed to drop from the syringe. Every care was taken to
36 avoid vibrations which could lead to the formation of a premature drop. Several of these drops
37 were formed and volume of one drop was obtained by taking the ratio of the total volume
38 displaced in the syringe to the total number of drops formed. The procedure for each
39 experimental data was repeated at least five times (but often 8-10 times) and the average value of
40 the drop volume was obtained. The relative standard deviation of high interfacial tension (>15)
41 was less than 2 % whereas for low interfacial tension was rarely as high as 4 % but often less
42 than 3 %.
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48 Interfacial tensions of 10 binary water-organic systems were studied near room temperature. The
49 experiments for studying the effect of temperature on interfacial tension were conducted, for five
50 binary water-organic systems, between 283.15 K and 333.15 K. For observing the effect of
51 solute concentration, propionic acid concentration (w_{HP}) in water was varied between 0 to 0.25
52 weight fraction and interfacial tensions of 4 water-organic systems were studied. All the
53 experiments were conducted at ambient pressure. The information such as purity, water content,
54 and the supplier regarding the chemicals used in the present work is given in Table 1. All the
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chemicals were used as received without any further purification. All solutions are prepared gravimetrically using a mass balance with $\pm 10^{-4}$ g.

Results and Discussion

The following expression was used for calculating the interfacial tension of a given system after experimentally finding the drop volume of the system:

$$\gamma_0 = \frac{(\rho_h - \rho_l) \cdot g \cdot V_d}{2 \cdot \pi \cdot r_C \cdot F} \quad (1)$$

where, γ_0 is initial interfacial tension, ρ_h is density of heavy phase, ρ_l is density of light phase, g is acceleration due to gravity, V_d is volume of a single drop, r_C is radius of the tip of the needle, and F is correction factor mentioned above that accounts for the drop portion that does not fall with the drop. It is important to mention that the representative radius used in Eqs 1–4 for the needle needs special attention²⁸. Often the studies do not explicitly pay attention to the fact that if they have to use outer radius, the needle material must be completely wettable with all of the liquids studied and by introducing some roughness²⁸ in the tip of needle cut perpendicularly. It may be useful to pay attention to the hydrophobicity (and hydrophilicity) of the needle-tip surface to determine the characteristic radius. Ideally outer radius should be used but for completely wetted tip-cut surface. We conducted a series of experiments with different systems reported in the literature, and found out that for a clean- and perpendicular- cut needle, the most suitable characteristic radius is average of internal and external radii.

The densities used in Eq. 1 were not that of mutually saturated phases, but are those of pure components and pure aqueous solutions of propionic acid. For any required temperature, the densities for 1-octanol, n-butyl acetate, ethyl acetate, diethyl ether, and propionic acid aqueous solutions at different mole fractions were obtained by curve fitting the literature data while densities of toluene, methylcyclohexane, cyclohexanone, and cyclohexanol were measured using the Rudolph Research Analytical vibrating tube automatic density meter. As part of our experimental method, the radius of tip (r_C) was taken as the average of outer and inner radius of the needle, as explained earlier. The following equations were used for calculating the correction factor $F^{28,29}$; different empirical correlations are recommended for different sizes of capillary needles and drops:

$$F = f\left(\frac{r_C}{\sqrt[3]{V_d}}\right) = 0.998 - 1.073\left(\frac{r_C}{\sqrt[3]{V_d}}\right), \quad 0.06 < \frac{r_C}{\sqrt[3]{V_d}} < 0.17 \quad (2)$$

$$F = f\left(\frac{r_C}{\sqrt[3]{V_d}}\right) = 0.992 - 1.2355\left(\frac{r_C}{\sqrt[3]{V_d}}\right) + 1.161\left(\frac{r_C}{\sqrt[3]{V_d}}\right)^2, \quad 0.17 < \frac{r_C}{\sqrt[3]{V_d}} < 0.30 \quad (3)$$

$$F = f\left(\frac{r_C}{\sqrt[3]{V_d}}\right) = \left(2 \times \pi \left(0.14782 + 0.27896\left(\frac{r_C}{\sqrt[3]{V_d}}\right) - 0.1662\left(\frac{r_C}{\sqrt[3]{V_d}}\right)^2\right)\right)^{-1}, \quad 0.3 < \frac{r_C}{\sqrt[3]{V_d}} < 1.2 \quad (4)$$

Because of the empirical nature of factor F in Eq 1, the reader will find different correlations in the literature for the correction factor, we particularly found out that the equation compiled by Drelich et al.³⁰ is only applicable to a limited range ($r_C/V_d^{1/3} \geq 0.30$), contrary to their description that suggests if it is a general case, which is somewhat misleading.

Binary initial interfacial tensions

Initial interfacial tensions of 10 binary organic-water systems are measured and reported in Table 2 along with the literature values for these systems where the literature values are those of mutually saturated phases. The initial interfacial tensions are expected to be different from the interfacial tensions because of the different densities used in Eq. 1 in the two cases, different interfacial associations in mutually saturated phases and initially pure phases, and the occurrence of any chemical reaction such as hydrolysis in the case of esters. Table 1 shows that apart from methylcyclohexane the initial interfacial tensions measured are fairly close to the literature values of interfacial tensions though it is expected that the measured initial interfacial tensions for substances that have relatively high mutual solubility with water are expected to have a relatively different value than the interfacial tensions measured when the phases are mutually saturated. On the other hand, the substances which have negligible solubility in water are expected to have virtually the same values of the two types of interfacial tensions. The cases for methylcyclohexane and cyclohexanol need some explanation. In the present work, the initial interfacial tension of methylcyclohexane with water is measured at 293.15 K as 51.40 mN/m while the literature⁵ value is 41.9 mN/m at 298.15 K. As suggested by Apostoluk and Drzymala³¹, the literature value of 41.9 mN/m is not possible and should be between 50–51 mN/m, because the other similar naphthenes such as cyclohexane (50.0 mN/m at 298.15 K)¹ and decalin (cis-decalin, 51.24 mN/m at 288.15 K)¹ have interfacial tensions with water in this range. Moreover, saturated alkanes such as n-hexane and n-heptane also have interfacial tensions as 51.1 mN/m at 293.15 K and 50.2 at 298.15 K¹, respectively. Also, Frietes et al.²⁷ have predicted the value of methylcyclohexane as 50.8 mN/m at 293.15 K while Apostoluk and Drzymala²² have predicted the value equal to 49.61 mN/m. As methylcyclohexane has only negligible solubility with water therefore the initial interfacial tension measured in this work may be regarded as the interfacial tension between the mutually saturated phases and should be a part of

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3 the interfacial tension database. For the case of cyclohexanol, it is important to mention that
4 cyclohexanol has melting point of 299.08 K²³ therefore the interfacial tension value of 3.92
5 mN/m¹ at 289.35 K is doubtful though mutual saturation with water may lead the possibility, it
6 however, should be checked. Interfacial tension of diethyl ether-water may also need to be
7 confirmed. For diethyl ether-water system, Backes et al.⁵ and Donahue and Bartell⁷ have found a
8 value of 11.0 mN/m at 298.15 K, Demond and Lindner¹ have reported a value of 10.7 mN/m at
9 293.15 K, Santos et al.¹³ have also worked out a value of 10.7 but at 303.15 K, and Kwok et al.¹¹
10 measured a value of 7.36 mN/m at 298.15 K compared to initial interfacial tension of 9.03 mN/m
11 at 293.15 K measured in the present study.
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17 18 **Effect of composition on initial interfacial tension**

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20 The effect of propionic acid concentration in aqueous solution on the initial interfacial tension
21 for 4 water-organic systems is provided in Table 3 and graphically shown in Fig. 2. It is observed
22 that varying the solute concentration in the aqueous phase significantly affects the initial
23 interfacial tension and for all the cases of the experimentation, initial interfacial tension appears
24 to decrease with an increase in the solute concentration. Initial interfacial tension without the
25 solute (propanoic acid) in the system, i.e., for the binary organic-water system is observed as the
26 maximum in all the cases. This may be due to the reason of decreased solubility of the
27 components in water. As the propanoic acid concentration increases in a system the mutual
28 solubility of the phases increases thereby decreases the interfacial surface (drop volume) as well
29 as the initial interfacial tension. The extent and trend of decrease in initial interfacial tension is
30 different in different systems depending may be on the initial interfacial tensions measured
31 without the solute presence or on the basis of different miscibility characteristics of propanoic
32 acid with an organic substance. Taking an example of toluene-water-propionic acid system, it is
33 observed from Fig. 2 that the rate of decrease of initial interfacial tension is quite large initially
34 as compared to the other systems and the rate decreases with an increase in propionic acid
35 concentration and may eventually lead to the region where all the three components are miscible.
36 The ternary initial interfacial data is fitted using the following exponential decay function (Eq. 5)
37 and the values of the parameters so obtained are given in Table 4 along with the corresponding
38 R² values. In each case, the t-value (t-value is a ratio of parameter value to its standard error) of
39 the parameters in was found well above 2.0.
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$$51 \quad \gamma_0 = a \exp(-bw_{HP_r}) \quad (5)$$

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53 where, a (mN/m) and b are constants and have to be obtained by fitting of the data and w_{HP_r} is
54 weight percent of propionic acid in water. Li and Fu¹⁰ have also observed a decrease in
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3 interfacial tension for the increase in propionic acid concentration when measured between
4 ternary phases of water + toluene + propionic acid.
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7 **Effect of temperature on initial interfacial tension**

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10 The effect of temperature on initial interfacial tension for five organic-water systems is shown in
11 Table 5 and Fig. 3. It is observed that the values of the initial interfacial tension are only slightly
12 affected by a change in temperature and the variation may be ignored in engineering
13 calculations. This phenomenon of reduced effect of temperature on interfacial tension has also
14 observed by other researchers in the field^{9,18,19}.
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18 **Conclusion**

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20 This work reports initial interfacial tensions of 10 organic-water binary systems. The organic
21 compounds include n-butyl acetate, cyclohexanol, cyclohexanone, diethyl ether, ethyl acetate,
22 methyl ethyl ketone, methylcyclohexane, 1-octanol, and toluene. Our initial interfacial tensions
23 are in agreement with the interfacial tensions measured in the literature for mutually saturated
24 phases whenever possible. The literature value of the interfacial tension of methylcyclohexane is
25 corrected and the measured initial interfacial tension is suggested to be included in the interfacial
26 tension database. The effect of propionic acid concentration in water and temperature on initial
27 interfacial tension of 4 organic-water system is measured. The solute addition has pronounced
28 effect on the initial interfacial tensions while the effect of temperature is found only marginal.
29 The method of initial interfacial tension measurement may not yield the exact value of interfacial
30 tensions especially for relatively highly mutually soluble phases but it is a rapid mean of
31 interfacial tension measurement close to the exact values as no mutual saturation is required till
32 equilibration and the densities of the mutually saturated phases are difficult to find in most of the
33 cases. The literature survey about the correlations for F correction factor finds that the
34 correlation compiled by Drelich et al.³⁰ is not universal but is applicable to a limited range of
35 volume.
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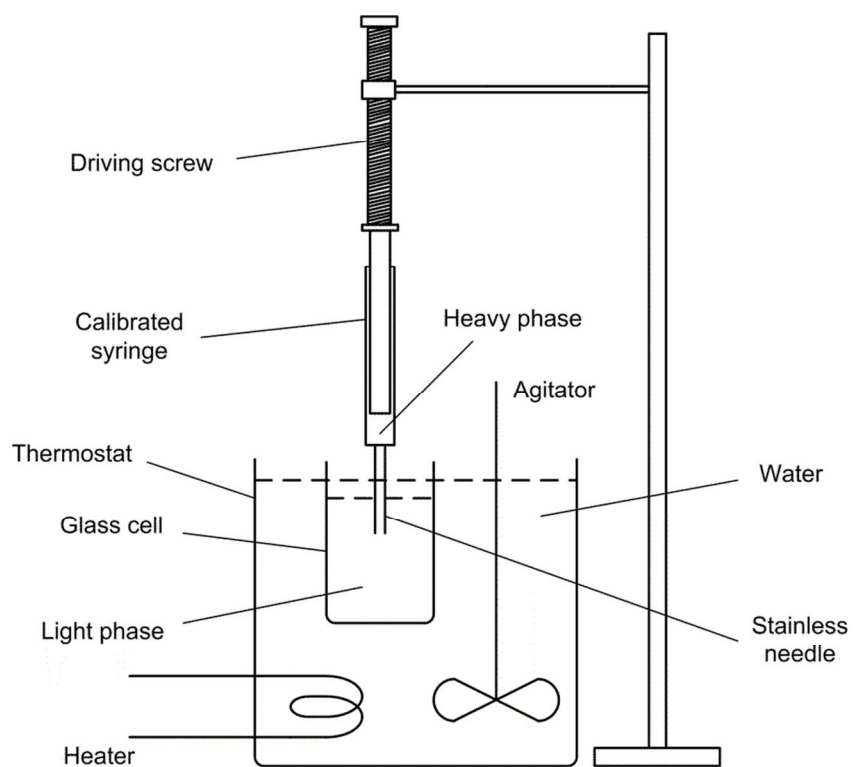


Fig. 1 Experimental setup (not to scale).

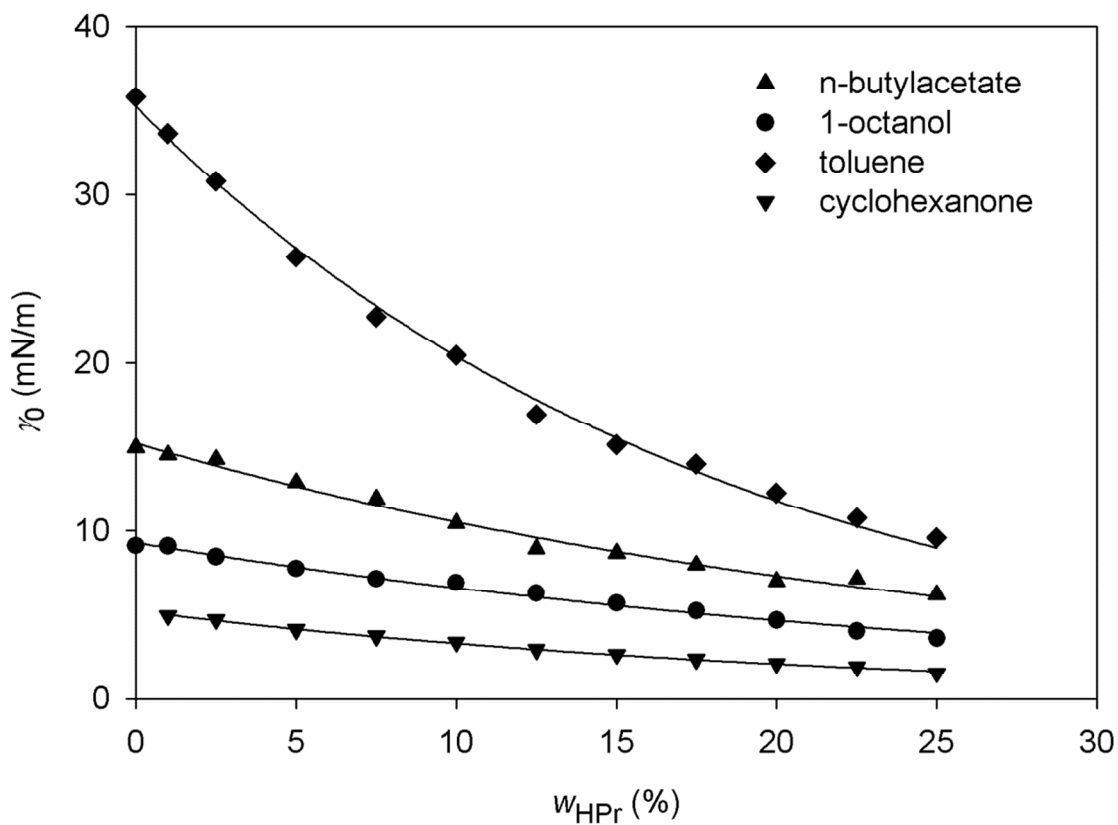


Fig. 2 Effect of propionic acid concentration on the initial interfacial tension of various water-organic systems. Solid lines show the model results given by Eq. 5.

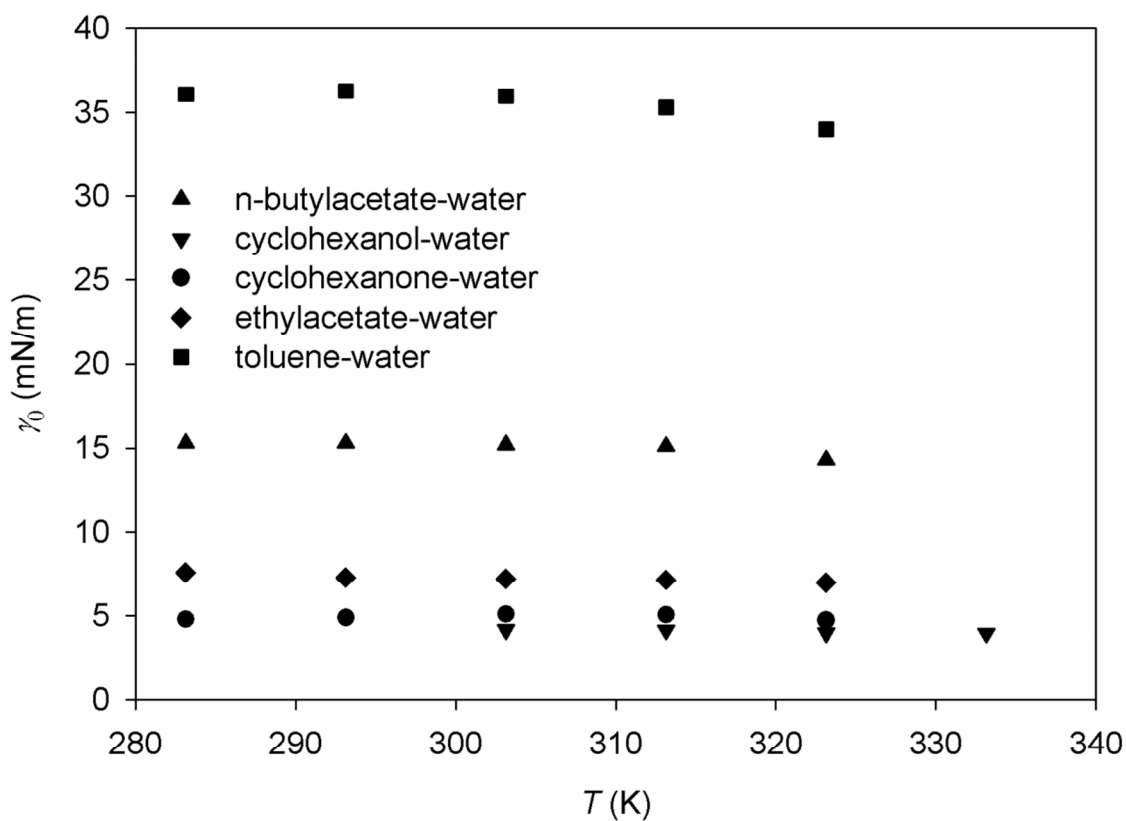


Fig. 3 Effect of temperature on the initial interfacial tension of various water-organic systems.

Table 1 Details of the chemicals used in the present study

Product	CAS Number	Chemical formula	Purity (wt%)	Water content (wt%)	Supplier
n-butyl acetate	123-86-4	C ₆ H ₁₂ O ₂	99	0.05	Lab-Scan
cyclohexanol	108-93-0	C ₆ H ₁₂ O	≥98	–	Fluka Chemika
cyclohexanone	108-94-1	C ₆ H ₁₀ O	>99	<0.2	Merck
diethyl ether	60-29-7	C ₄ H ₁₀ O	≥99.5	≤0.2	Riedel-de Haën
ethyl acetate	141-78-6	C ₄ H ₈ O ₂	>99	<0.1	Merck
methyl cyclohexane	108-87-2	C ₇ H ₁₄	≥99	anhydrous	Sigma-Aldrich
methyl ethyl ketone	78-93-3	C ₄ H ₈ O	99.5	0.1	Lab-Scan
1-octanol	111-87-5	C ₈ H ₁₈ O	99	0.1	Panreac Sintesis
toluene	108-88-3	C ₇ H ₈	≥99.5	≤0.05	Riedel-de Haën
water, de-ionized	7732-18-5	H ₂ O	100	100	Local market

Table 2 Experimental initial interfacial tension of various organic-water systems at ambient pressure (101 kPa)

System	This work γ_0 (mN/m) ^a	T (K)	Literature γ (mN/m)	T (K)	S^{32} g/L-H ₂ O	T (K)
n-butyl acetate	14.95	290.15	14.5 ⁷	298.15	6.80	293.15
cyclohexanol	4.17	303.15	3.7 ⁵	298.35	40.0	298.15
cyclohexanone	4.87	293.15	3.9 ⁵	293.85	96.0	298.15
diethyl ether	9.03	293.15	10.70 ¹ 7.36 ¹¹	293.15 298.15	64.2	298.15
ethyl acetate	7.37	289.15	6.8 ¹	298.15	87.9	298.15
methyl ethyl ketone	0.92 ^b	292.15	1.0 ²⁰	298.15	~210	298.15
methylcyclohexane	51.40	293.15	41.9 ⁵	298.15	0.015	298.15
1-octanol	9.10	289.15	8.52 ¹	293.15	0.540	298.15
Toluene	35.80	290.15	35.4 ⁵	298.15	0.531	298.15

^aStandard uncertainties are $u(T) = 0.25$ K, $u(V) = 0.01$ cm³. Expanded uncertainty for the initial interfacial tension (γ_0) is $U(c) = 0.50$ mN/m (0.95 level of confidence). ^bonly measured for once. γ_0 , initial interfacial tension; γ , interfacial tension (of mutually saturated phases); s , solubility of organic component in water; T , temperature of measurement.

Table 3 Effect of propionic acid concentration in water on the initial interfacial tension of various organic-water systems at ambient pressure (101 kPa)

w_{HP_r} (wt%)	x_{HP_r}	γ_0 (mN/m) ^a			
		n-butyl acetate	cyclohexanone	1-octanol	toluene
		$T = 289.15$ K	$T = 289.15$ K	$T = 289.15$ K	$T = 290.15$ K
0.0	0.0	14.9	–	9.10	35.8
1.0	0.0025	14.5	4.92	9.08	33.6
2.5	0.0062	14.2	4.70	8.43	30.8
5.0	0.0126	12.9	4.10	7.73	26.3
7.5	0.0193	11.9	3.73	7.12	22.8
10.0	0.0263	10.5	3.35	6.90	20.4
12.5	0.0336	8.92	2.92	6.26	16.9
15.0	0.0412	8.66	2.63	5.67	15.1
17.5	0.0491	7.95	2.35	5.20	13.9
20.0	0.0573	6.99	2.11	4.67	12.2
22.5	0.0660	7.12	1.89	4.02	10.7
25.0	0.0750	6.18	1.53	3.59	9.57

^aStandard uncertainties are $u(x) = 0.0001$, $u(T) = 0.25$ K, $u(V) = 0.01$ cm³. Expanded uncertainty for the initial interfacial tension (γ_0) is $U(c) = 0.50$ mN/m (0.95 level of confidence). x_{HP_r} is mole fraction of propionic acid in water.

Table 4 Parameters of Eq. 5 fitted for ternary propionic acid- organic solvent-water systems

	Parameter values			
	n-butyl acetate	cyclohexanone	1-octanol	toluene
a (mN/m)	15.1977	4.9480	9.2911	35.2570
b	0.0368	0.0421	0.0346	0.0548
R^2	0.9892	0.9975	0.9892	0.9967

Table 5 Effect of temperature on the initial interfacial tension of various water-organic systems at ambient pressure (101 kPa)

T (K)	n-butyl acetate	cyclohexanol	cyclohexanone	ethyl acetate	toluene
γ_0 (mN/m) ^a					
283.15	15.3	–	4.78 ^b	7.61	36.1
293.15	15.3	–	4.87	7.29	36.3
303.15	15.2	4.17	5.08	7.19	36.0
313.15	15.1	4.15	5.05	7.15	35.3
323.15	14.3	3.97	4.71	6.99	34.0
333.15	–	3.95	–	–	–

^aStandard uncertainties are $u(T) = 0.25$ K, $u(V) = 0.01$ cm³. Expanded uncertainty for the initial interfacial tension (γ_0) is $U(c) = 0.50$ mN/m (0.95 level of confidence). ^bOnly measured for once.

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TOC Graphic

